

Optimization of preparation conditions for rice husk based activated carbons for the removal of methylene blue dye

Murat MN¹, Mohd Azmier Ahmad^{1,3*} and Mohd Nazri Idris²

¹School of Chemical Engineering, Engineering Campus, Universiti Sains Malaysia, 14300 Nibong Tebal, Penang, Malaysia

²Solid Waste Management Cluster, Science & Engineering Research Centre, Engineering Campus, Universiti Sains Malaysia, Nibong Tebal, Penang, Malaysia

³School of Materials and Mineral Resources Engineering, Engineering Campus, Universiti Sains Malaysia, 14300 Nibong Tebal, Penang, Malaysia

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***Corresponding author:**

Mohd Azmier Ahmad

School of Chemical Engineering
Engineering Campus, Universiti Sains
Malaysia

14300 Nibong Tebal

Penang, Malaysia

Tel: +604 5996459

Fax: +604 5996908

E-mail: chazmier@usm.my

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Abstract

This study investigates the optimal conditions for preparation of rice husk based activated carbon (RHAC) using carbon dioxide gasification of rice husk char under microwave irradiation. The central composite design (CCD) was used to determine the effects of the two preparation variables; microwave power and activation time on MB removal and RHAC yield. Based on the CCD, a quadratic model and linear models were developed for MB removal and RHAC yield, respectively. The significant factors on each experimental design response were identified from the analysis of variance (ANOVA). The optimum conditions for RHAC preparation were obtained by using activation time of 4.28 min and microwave power of 440 W, which resulted MB removal of 83.05% and RHAC yield of 31.98%.

Keywords: Activated carbon, Adsorption, Methylene blue, Microwave heating, Optimization, Rice husk

Introduction

The textile industry uses dyes to color their product consume large quantities of water [1]. More than 100,000 commercially available dyes with over 7×10^5 tonnes of dyestuff produced every year have been estimated [2]. At the same time, massive amount of textile wastewater is produced during dyeing and finishing processes. One of the serious issues associated with textile wastewater is colored effluent as they produce an obvious color to water even at low concentration [3]. Therefore, the appearance of dyes onto streams and rivers are categorized as threatening pollutant that should not be neglected. Indeed, removal of dyes from the effluent before its disposal in water bodies is very important [4]. In the last few years, great attention has been placed on utilizing waste as precursor for producing low-cost activated carbon. In this study an attempt was made to find the optimum preparation condition of producing activated carbon from rice husk waste.

Methodology

The rice husk was placed in a Pyrex glass reactor in the chamber of the microwave oven. The microwave irradiation was carried at targeted radiation time and radiation power under carbon dioxide flow of 150 ml/min as suggested by the Design Expert software. The response surface methodology (RSM) design known as central composite design (CCD) was used in this study. The variables involved were microwave power (x_1) and activation time (x_2) with MB removal (y_1) and RHAC yield (y_2) as responses. The code levels for CCD are shown in Table 1.

Table 1. Independent variables and their coded levels for the CCD

Variables (factors)	Coded variables level				
	$-\alpha$	-1	0	+1	$+\alpha$
Microwave power (W)	191	264	440	616	689
Activation time (min)	3.17	4.00	6.00	8.00	8.83

Results and discussion

The response values that obtained from the experimental works using the design of expert software are shown in Table 2. The polynomial regression equation was developed using CCD. As suggested by the software, the quadratic and linear models were selected for MB removal (Y_1) and RHAC yield (Y_2), respectively as the best model to correlate the data to the response.

Table 2. Response values of the experimental works

RHAC preparation variable		MB removal, Y_1 (%)	RHAC yield, Y_2 (%)
Microwave power, x_1 (W)	Activation time, x_2 (min)		
440	6.00	89.95	27.00
616	8.00	91.61	26.67
264	8.00	79.42	34.00
440	8.83	90.18	25.67
440	6.00	89.11	27.67
440	6.00	90.46	28.00
616	4.00	90.59	27.00
440	3.17	73.67	31.33
440	6.00	90.54	29.00
689	6.00	94.12	19.00
191	6.00	70.96	44.33
264	4.00	72.79	36.60
440	6.00	89.90	28.00

The final empirical models for MB removal and RHAC in term of coded factors are shown in Equation Equations 1 and 2 respectively,

The correlation coefficient, R^2 value were used to evaluate the suitability of model equation. The model developed is the best at low standard deviation and high R^2 statistic which is closer to the unity. The R^2 values for Equations 1 and 2 were 0.9546 and 0.9052, respectively. The higher R^2 values indicate that the predicted values for MB removal and RHAC were closer to its actual value [5].

Analysis of variance (ANOVA) was carried out to justify the adequacy of the models. The ANOVA for the quadratic model of MB removal is shown in Table 3, where the F-value of 29.45 and Prob>F is 0.0001 prove that the model is significant. The microwave power (x_1), activation time (x_2), quadratic term of microwave power (x_1^2) and the quadratic terms of activation time (x_2^2) were significant model terms whereas the interaction terms (x_1x_2) were insignificant to the response.

Table 3. ANOVA for MB removal by RHAC

Source	Sum of squares	Degree of freedom (DF)	Mean square	F-Value	Prob.>F
Model	774.44	5	154.89	29.45	0.0001
x_1	492.09	1	492.09	93.55	<0.0001
x_2	120.11	1	120.11	22.83	0.0020
x_1x_2	7.87	1	7.87	1.50	0.2609
x_1^2	79.64	1	79.64	15.14	0.0060
x_2^2	94.77	1	94.77	18.02	0.0038

Table 4 shows the ANOVA for quadratic model for RHAC yield. The model F-value of 17.65 and Prob>F of 0.0005 indicates the model is significant. Based on the result obtained, microwave power (x_1) and the activation time (x_2) were significant model terms.

Table 4. ANOVA for RHAC yield

Source	Sum of squares	Degree of freedom	Mean square	F-Value	Prob.>F
Model	339.18	2	169.59	17.65	0.0005
x_1	287.32	1	287.32	29.90	0.0003
x_2	51.09	1	51.85	5.40	0.0426

Three-dimensional surface response and contour plots were constructed to assess the interactive relationships between independent variables and responses of certain models. Figure 1 shows three-dimensional surface responses for two factors microwave power and activation time on MB removal.

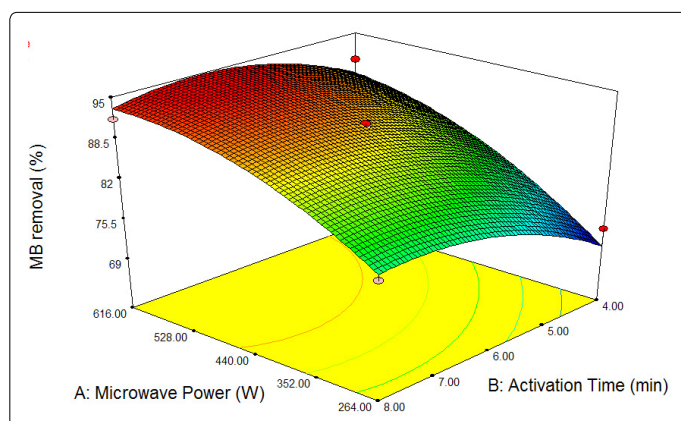


Figure 1. Three-dimensional response surface plot of MB removal by RHAC

High microwave power promotes the development of pores on the sample, thus resulted high response value. Figure 2 shows the three-dimensional response surface of the combined effect of microwave power and activation time on the RHAC yield. All variable were significant on the response with microwave power imposing greater effect than activation time. Increase the microwave power, significantly more pores and active site were developed on the RHAC surface. Therefore the yield decreases with increasing activation time due to more release of volatile matter.

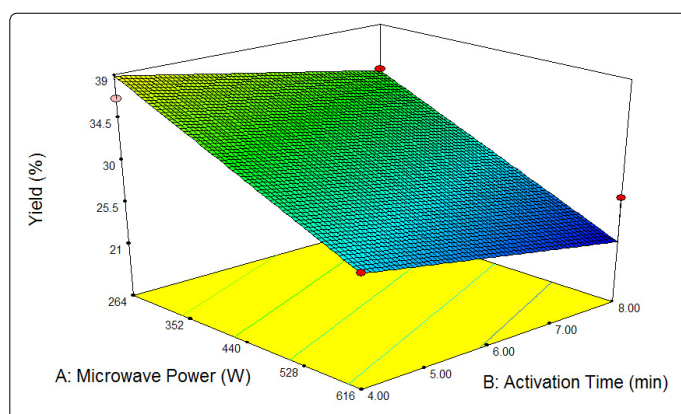


Figure 2. Three-dimensional response surface plot of RHAC yield

The aim of this study is to obtain the optimum parameters of RHAC produced with highest RHAC yield and MB removal. Design Expert software was used to compromise between yield and MB removal while optimizing both of these values by selecting the highest responses from the experimental result. The optimum operating conditions is depending on achieving high MB removal. The experimental conditions with the highest desirability are shown in the Table 5.

Table 5. Model validation for MB removal and RHAC yield

Microwave power, x_1 (W)	Activation time, x_2 (min)	MB removal (%)			RHAC yield (%)		
		Predicted	Experimental	Error (%)	Predicted	Experimental	Error (%)
440	4.28	83.93	83.05	1.05	32.55	31.98	1.75

The optimum preparation conditions were obtained at activation time of 4.28 min and microwave power of 440 W, which resulted MB removal of 83.05% and RHAC yield of 31.98%. The error for the MB removal and RHAC yield between the experimental and predicted value are 1.05% and 1.75%, respectively, which indicates sufficient accuracy of the process optimization.

Conclusion

Response surface methodology was successfully used to investigate the effects of microwave power and activation time on the MB removal and RHAC yield. The optimum RHAC preparation conditions were obtained using activation time of 4.28 min and microwave power of 440 W, which resulted MB removal of 83.05% and RHAC yield of 31.98%. Through analysis of the response surface, microwave power and activation time were found to have significant effects on MB removal and RHAC yield.

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